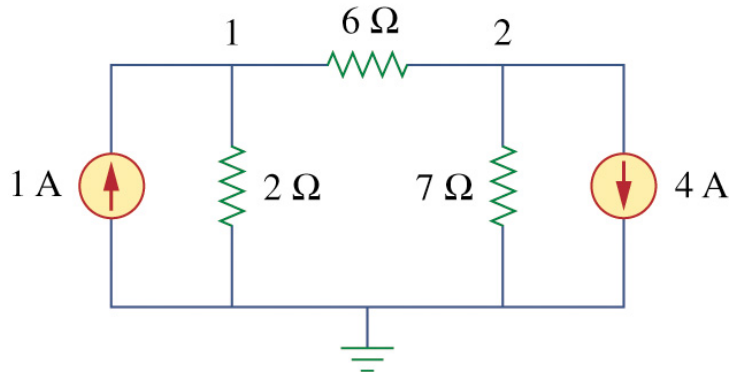


**1.**

Obtain the node voltages in this circuit using nodal analysis by inspection. Remember that the coefficients in the matrix are *conductances*, not *resistances*. Use MATLAB to solve for the node voltage values.



$$\begin{bmatrix} \frac{1}{2} + \frac{1}{6} & -\frac{1}{6} \\ -\frac{1}{6} & \frac{1}{6} + \frac{1}{7} \end{bmatrix} \begin{bmatrix} v_1 \\ v_2 \end{bmatrix} = \begin{bmatrix} 1 \\ -4 \end{bmatrix}$$

```
>> A=[1/2+1/6 -1/6;-1/6 1/6+1/7];
```

```
>> b=[1;-4];
```

```
>> vv=A\b; % "\" "divides" by A on the left, that is A^(-1)b
```

```
>> vv
```

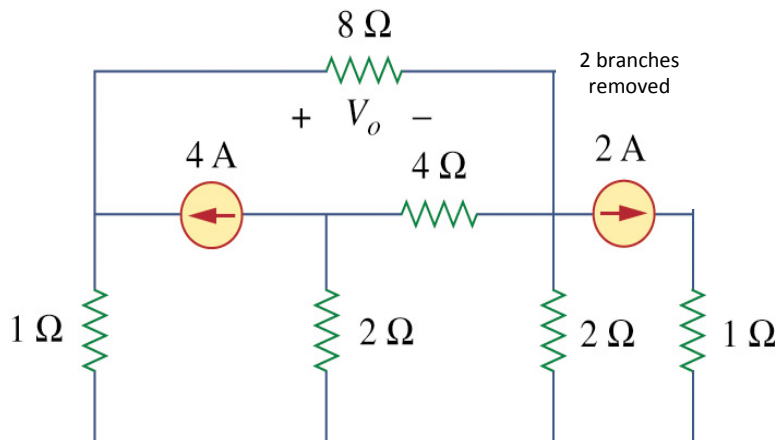
```
vv =
```

```
    -2
```

```
   -14
```

**2:** Use nodal analysis by inspection and then find  $V_o$  in the following circuit (updated 2/9/2017).

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$$V_o = v_1 - v_2$$

$$\begin{bmatrix} \frac{1}{1} + \frac{1}{8} & 0 & -\frac{1}{8} & 0 \\ 0 & \frac{1}{2} + \frac{1}{4} & -\frac{1}{4} & 0 \\ -\frac{1}{8} & -\frac{1}{4} & \frac{1}{4} + \frac{1}{2} + \frac{1}{8} & 0 \\ 0 & 0 & 0 & \frac{1}{1} \end{bmatrix} \begin{bmatrix} v_1 \\ v_2 \\ v_3 \\ v_4 \end{bmatrix} = \begin{bmatrix} 4 \\ -4 \\ -2 \\ 2 \end{bmatrix}$$

```
>> A=[1/1+1/8, 0, -1/8, 0;
      0, 1/2+1/4, -1/4, 0;
      -1/8, -1/4, 1/4+1/2+1/8, 0;
      0, 0, 0, 1/1]
```

```
A =
    1.1250    0 -0.1250    0
    0    0.7500 -0.2500    0
   -0.1250  -0.2500  0.8750    0
    0    0    0    1.0000
```

```
>> b=[4;-4;-2;2];
```

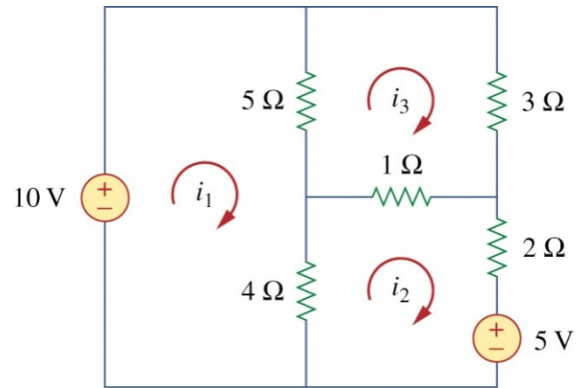
```
>> vv=A\b
```

```
vv =
```

```
    3.1429
   -6.5714
   -3.7143
    2.0000
```

3.

Obtain the matrix equation for the mesh currents in the circuit at the right by inspection, then solve for the mesh currents using MATLAB.



$$\begin{bmatrix} 5+4 & -4 & -5 \\ -4 & 4+1+2 & -1 \\ -5 & -1 & 5+1+3 \end{bmatrix} \begin{bmatrix} i_1 \\ i_2 \\ i_3 \end{bmatrix} = - \begin{bmatrix} -10 \\ 5 \\ 0 \end{bmatrix} = \begin{bmatrix} 10 \\ -5 \\ 0 \end{bmatrix}$$

```
>> A=[5+4 -4 -5;
      -4 4+1+2 -1;
      -5 -1 5+1+3]
```

A =

```
9 -4 -5
-4 7 -1
-5 -1 9
```

```
>> b=[-10;5;0]
```

b =

```
10
-5
0
```

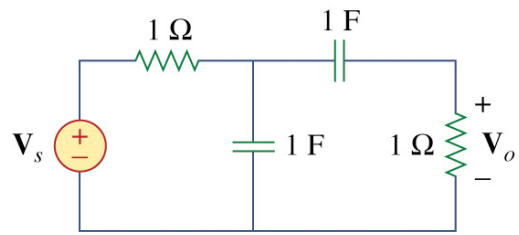
```
>> ii=A\b
```

ii =

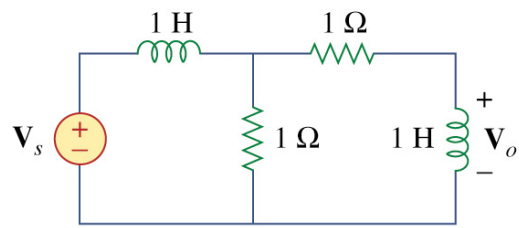
```
2.0854
0.6533
1.2312
```

4. Determine the center frequency and the bandwidth of the frequency selective circuits in the following figure. You may use inspection techniques if your wish. Treat  $\mathbf{H}(\omega) = \frac{\mathbf{V}_o(\omega)}{\mathbf{V}_i(\omega)}$  and apply the condition for resonance.

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(a)



(b)

I apologize. This, again, is a not-completely-defined problem from the textbook.

Let  $\mathbf{H}(\omega) = \frac{\mathbf{V}_o(\omega)}{\mathbf{V}_s(\omega)}$  (this is the part that was missing).

Find the center frequency and bandwidth of the circuit in (a)

Define  $\mathbf{I}$  as the current flowing out of the source  $\mathbf{V}_s$ . By Ohm's Law,  $\mathbf{I} = \frac{\mathbf{V}_s}{\mathbf{Z}_T}$ ,

where  $\mathbf{Z}_T$  is total impedance of the circuit.  $\mathbf{Z}_T = R + \frac{1}{j\omega C} \parallel \left( R + \frac{1}{j\omega C} \right)$ , where  $R = 1\Omega$  and  $C = 1\text{F}$

Switch to  $s$  for ease of notation,  $\mathbf{Z}_T = R + \frac{1}{sC} \parallel \left( R + \frac{1}{sC} \right) = R + \frac{1}{sC} \parallel \left( \frac{1+sRC}{sC} \right)$

$$\begin{aligned} &= R + \frac{\frac{1}{sC} \left( \frac{1+sRC}{sC} \right)}{\frac{1}{sC} + \left( \frac{1+sRC}{sC} \right)} = R + \frac{\frac{1}{s^2 C^2} (1+sRC)}{\left( \frac{2+sRC}{sC} \right)} = R + \frac{(1+sRC)}{sC(2+sRC)} \\ &= \frac{RsC(2+sRC) + (1+sRC)}{sC(2+sRC)} = \frac{(2sRC + s^2 R^2 C^2) + (1+sRC)}{sC(2+sRC)} = \frac{(1+3sRC + s^2 R^2 C^2)}{sC(2+sRC)} \end{aligned}$$

$$\mathbf{I} = \frac{\mathbf{V}_s}{\mathbf{Z}_T} = \frac{\mathbf{V}_s sC(2+sRC)}{(1+3sRC + s^2 R^2 C^2)} \quad \text{Don't worry about the math yet!}$$

$\mathbf{V}_o = \mathbf{I}_1 \times R$ , where  $\mathbf{I}_1$  is the current in the  $R + \frac{1}{sC}$  branch. This is a current divider,

$$\text{so } \mathbf{I}_1 = \frac{\frac{1}{sC}}{\frac{1}{sC} + R + \frac{1}{sC}} \mathbf{I} = \frac{\mathbf{I}}{2+sRC} = \frac{1}{2+sRC} \times \frac{\mathbf{V}_s sC(2+sRC)}{(1+3sRC + s^2 R^2 C^2)}$$

$$\mathbf{V}_o = \mathbf{I}_1 R = \frac{\mathbf{V}_s sRC}{(1+3sRC + s^2 R^2 C^2)}, \text{ so } \mathbf{H}(s) = \frac{\mathbf{V}_o}{\mathbf{V}_s} = \frac{sRC}{(1+3sRC + s^2 R^2 C^2)}$$

Just checking that I did everything right,  $s$  has units of  $\text{sec}^{-1}$ ,  $RC$  is  $\text{sec}$ , so we

$$\text{have } \mathbf{H}(\omega) = \frac{\text{sec}^{-1} \text{sec}}{(1 + \text{sec}^{-1} \text{sec} + \text{sec}^{-2} \text{sec}^2)} = \frac{1}{1} \text{ which is OK for } \frac{\text{volts}}{\text{volt}}$$

Look at the denominator, and rearrange in our standard form as a monic polynomial with 1 as the coefficient of the highest power of  $s$ :

$$\mathbf{H}(s) = \frac{sRC}{(R^2 C^2) \left( s^2 + \frac{3sRC}{R^2 C^2} + \frac{1}{R^2 C^2} \right)} = \frac{s/(RC)}{\left( s^2 + \frac{3s}{RC} + \frac{1}{R^2 C^2} \right)} \text{ with units of } \frac{\text{sec}^{-2}}{\text{sec}^{-2}}.$$

$$\text{From our standard form, } \alpha = \frac{3}{2RC} \quad \omega_0 = \frac{1}{RC}.$$

$$\text{So the center frequency is } \omega_0 = \frac{1}{1\Omega \times 1\text{F}} = 1 \text{ r/s. } B = 2\alpha = \frac{2 \times 3}{2RC} = \frac{3}{1\Omega \times 1\text{F}} = 3 \text{ r/s.}$$

the process is the same for this problem

$$\mathbf{Z}_T = sL + (R \parallel R + sL) = sL + \frac{R(1+sL)}{R+R+sL} = sL + \frac{(R+sL)}{\left(2+s\frac{L}{R}\right)} = \frac{2sL + s^2\frac{L^2}{R} + R + sL}{\left(2+s\frac{L}{R}\right)}$$

$$= \frac{R\left(s^2\frac{L^2}{R^2} + 3s\frac{L}{R} + 1\right)}{\left(2+s\frac{L}{R}\right)} \text{ we'll simplify later.}$$

$$\mathbf{I} = \frac{\mathbf{V}_s\left(2+s\frac{L}{R}\right)}{R\left(s^2\frac{L^2}{R^2} + 3s\frac{L}{R} + 1\right)}, \mathbf{I}_1 = \mathbf{I} \times \frac{R}{(2R+sL)} = \mathbf{I} \times \frac{1}{\left(2+s\frac{L}{R}\right)}$$

$$= \frac{\mathbf{V}_s\left(2+s\frac{L}{R}\right)}{R\left(s^2\frac{L^2}{R^2} + 3s\frac{L}{R} + 1\right)} \times \frac{1}{\left(2+s\frac{L}{R}\right)} = \frac{\mathbf{V}_s}{R\left(s^2\frac{L^2}{R^2} + 3s\frac{L}{R} + 1\right)}$$

$$\mathbf{V}_o = sL\mathbf{I} = \frac{\mathbf{V}_s sL}{R\left(s^2\frac{L^2}{R^2} + 3s\frac{L}{R} + 1\right)}$$

$$\mathbf{H}(s) = \frac{\mathbf{V}_o}{\mathbf{V}_s} = \frac{sL}{R\left(s^2\frac{L^2}{R^2} + 3s\frac{L}{R} + 1\right)} = \frac{s(L/R)}{\left(s^2\frac{L^2}{R^2} + 3s\frac{L}{R} + 1\right)} = \frac{s(L/R)}{\frac{L^2}{R^2}\left(s^2 + 3s\frac{R}{L} + \frac{R^2}{L^2}\right)}$$

$$\mathbf{H}(s) = \frac{s(R/L)}{\left(s^2 + 3s\frac{R}{L} + \frac{R^2}{L^2}\right)}.$$

Following the same process  $\omega_0 = \frac{R}{L} = 1 \text{ r/s}$ .  $\alpha = \frac{3R}{2L} = \frac{3}{2}$ ,  $B = 2\alpha = 3 \text{ r/s}$ .

Both problems seem WRONG, because  $\omega_0 \pm \frac{BW}{2}$  gives the half power (-3 dB) band edges as  $\omega_1 = -0.5$ , and we don't really know what a negative frequency means in this context.

BUT, the  $\omega_0 \pm \frac{BW}{2}$  approximation only holds when  $BW \ll \omega_0$ , which isn't the case here, so we have to back to the book (or lecture).

$\omega_0 = \sqrt{\omega_1 \omega_2}$ , the *geometric* mean, instead of the *arithmetic* mean.

$BW = \omega_2 - \omega_1 = 3$  rps, so  $\omega_2 = 3 + \omega_1$ . Substituting in the equation for  $\omega_0 = \sqrt{\omega_1(3 + \omega_1)}$ , or,  $\omega_0^2 = 3\omega_1 + \omega_1^2$ . Substituting the value of

$$\omega_0 = 1, \omega_1^2 + 3\omega_1 - 1 = 0, \omega_1 = \frac{-3 \pm \sqrt{9 - 4(-1)}}{2} = \frac{-3 \pm \sqrt{13}}{2}.$$

Discarding the negative root, because  $\omega_1 > 0$ ,  $\omega_1 = \frac{-3}{2} + \frac{\sqrt{13}}{2} = 0.3028$

$$\omega_2 = 3 + 0.3028 = 3.3028.$$

Just checking  $\omega_0 = 1 = \sqrt{0.3028(3.3028)} = 1!!$